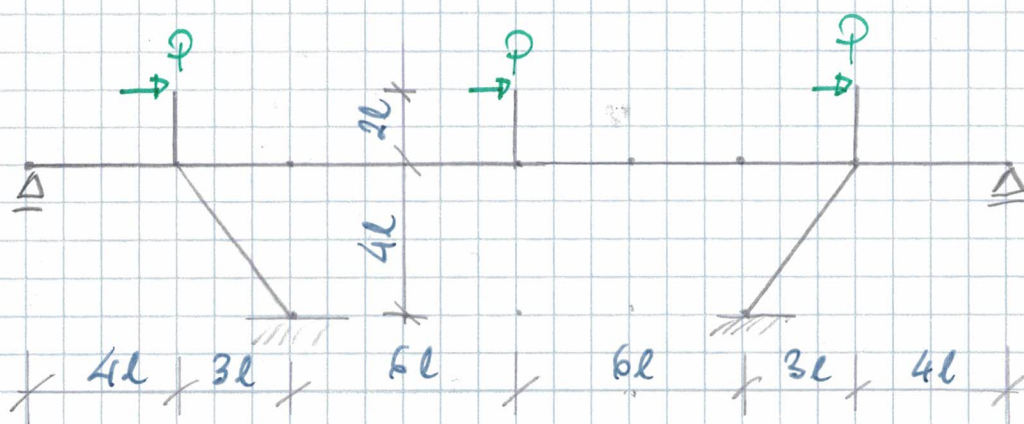
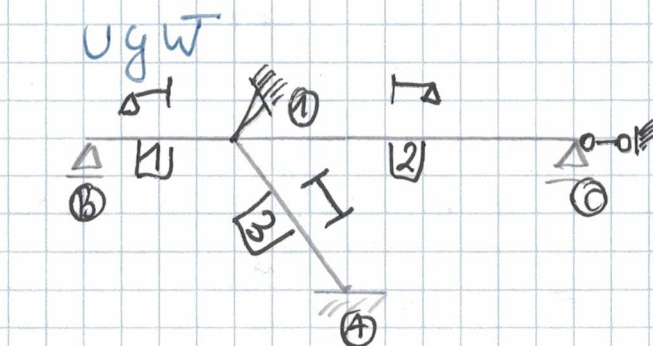
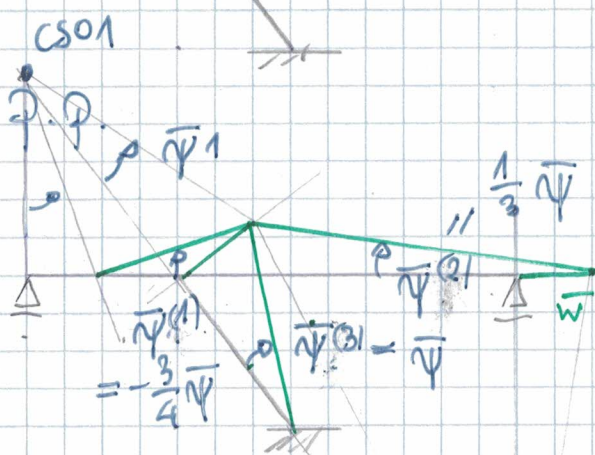
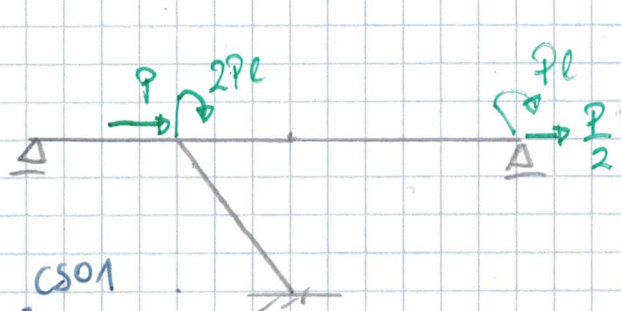


Kolokwium nr 2.2. MK1 r.a. 2024/25

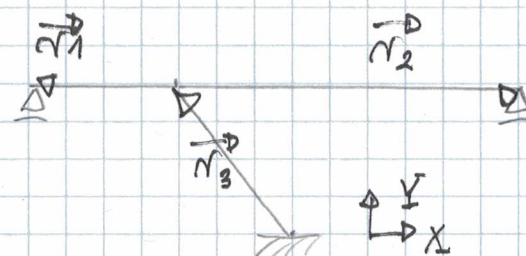


$Ey = \text{const.}$
 $EA = \text{const.}$
 $M = ?$

Schemat główny i redukcja cz. stat. wyznaczalnej



metoda analityczna



$$\vec{r}_3 = [-3l, 4l]$$

$$\vec{r}_1 = [-4l, 0]$$

$$\vec{r}_2 = [9l, 0]$$

$$u_{y1} : 0 = 0 + 3l \bar{\psi}^{(3)} + 4l \bar{\psi}^{(1)}$$

$$u_{y2} : 0 = 0 + 3l \bar{\psi}^{(3)} - 9l \bar{\psi}^{(2)}$$

$$\bar{\psi}^{(3)} = \bar{\psi}$$

$$\bar{\psi}^{(1)} = -\frac{3}{4} \bar{\psi}$$

$$\bar{\psi}^{(2)} = \frac{1}{3} \bar{\psi}$$

r. r. MP

$$\Phi_1^{(1)} + \Phi_1^{(2)} + \Phi_1^{(3)} = 2Pl \quad (1)$$

$$\Phi_1^{(1)} \left(-\frac{3}{4}\bar{\psi}\right) + (\Phi_1^{(3)} + \Phi_A^{(3)})\bar{\psi} + \Phi_1^{(2)} \left(\frac{1}{3}\bar{\psi}\right) + \bar{L}_{obc} = 0$$

$$\bar{L}_{obc} = Pl \cdot \frac{1}{3}\bar{\psi} + \frac{Pl}{2} \cdot \bar{\psi} \cdot 4l + Pl \cdot \bar{\psi} \cdot 4l = 6\frac{1}{3}Pl\bar{\psi}$$

$$\frac{3}{4}\Phi_1^{(1)} - (\Phi_1^{(3)} + \Phi_A^{(3)}) - \frac{1}{3}\Phi_1^{(2)} = 6\frac{1}{3}Pl \quad (2)$$

Momenty wywołane  $\Phi_1^{(2)} = \frac{Pl}{2}$

WT $\Phi_1^{(1)} = \frac{3EY}{4l} [\psi_1 + \frac{3}{4}\bar{\psi}] = \frac{EY}{l} [\frac{3}{4}\psi_1 + \frac{9}{16}\bar{\psi}] \quad (\frac{3}{4})$

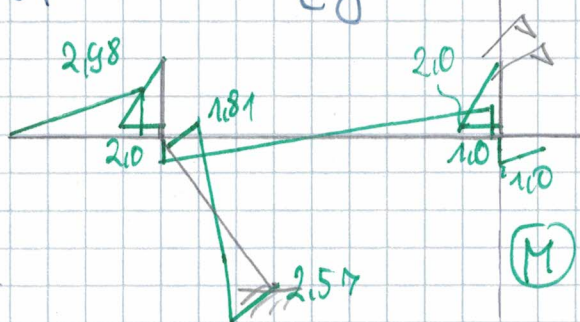
2) $\Phi_1^{(2)} = \frac{3EY}{9l} [\psi_1 - \frac{1}{3}\bar{\psi}] + \frac{Pl}{2} = \frac{EY}{l} [\frac{1}{3}\psi_1 - \frac{1}{9}\bar{\psi}] + \frac{Pl}{2} \quad (-\frac{1}{9})$

3) $\Phi_1^{(1)} = \frac{2EY}{5l} [2\psi_1 - 3\bar{\psi}] = \frac{EY}{l} [\frac{4}{5}\psi_1 - \frac{6}{5}\bar{\psi}]$
 $\Phi_A^{(1)} = \frac{EY}{l} [\frac{2}{5}\psi_1 - \frac{6}{5}\bar{\psi}] \quad (-1)$

$$\frac{EY}{l} \begin{bmatrix} \frac{3}{4} + \frac{1}{3} + \frac{4}{5} & \frac{9}{16} - \frac{1}{9} - \frac{6}{5} \\ \frac{9}{16} - \frac{1}{9} - \frac{6}{5} & \frac{27}{64} + \frac{1}{27} + \frac{12}{5} \end{bmatrix} \begin{bmatrix} \psi_1 \\ \bar{\psi} \end{bmatrix} = \begin{bmatrix} 2 - \frac{1}{2} \\ 6\frac{1}{3} + \frac{1}{6} \end{bmatrix} Pl$$

$$\psi_1 = 1.898 \frac{Pl^2}{EY}$$

$$\bar{\psi} = 2.771 \frac{Pl^2}{EY}$$

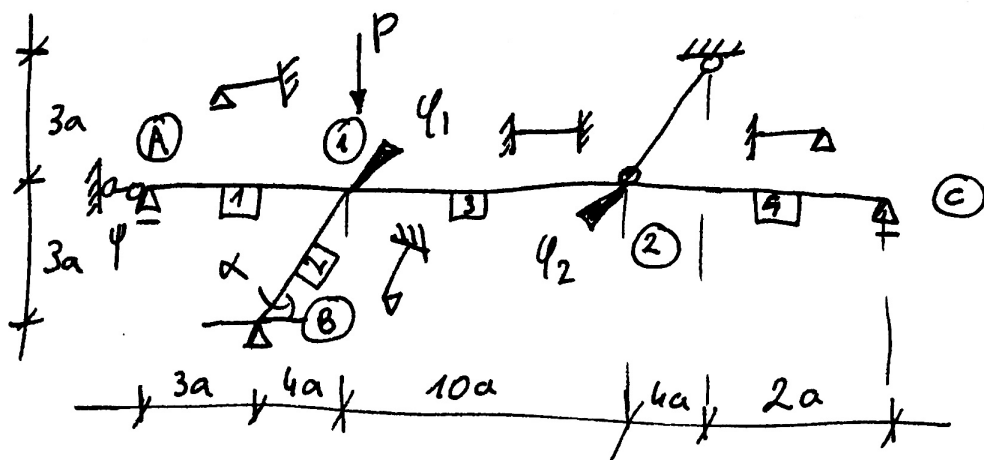


(M) [Pl]

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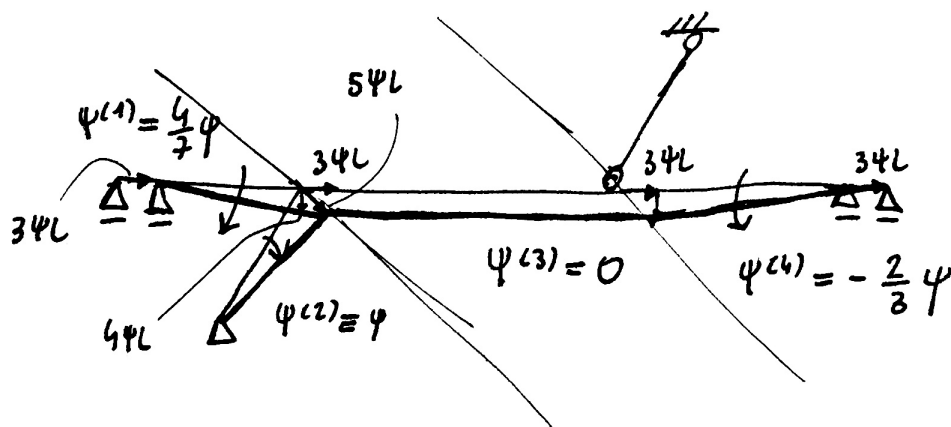
$$EA = \infty, EJ = \text{const.}; M = ?$$

SCHEMAT POŁÓWKOWY + UGW



$$q = \begin{bmatrix} \psi_1 \\ \psi_2 \\ \psi \end{bmatrix}$$

PLAN PRZEM. (CIĘCIWY PRĘTÓW)



$$\begin{cases} \psi^{(1)} = \frac{4}{7} \psi \\ \psi^{(2)} = \psi \\ \psi^{(3)} = 0 \\ \psi^{(4)} = -\frac{2}{3} \psi \end{cases}$$

RRMP:

$$\bar{L}_{\text{obc}} = 4 \psi L \cdot P$$

$$1) \phi_1^{(1)} + \phi_1^{(2)} + \phi_1^{(3)} = 0$$

$$2) \phi_2^{(3)} + \phi_2^{(4)} = 0$$

$$3) \phi_1^{(1)} \cdot \frac{4}{7} \bar{\psi} + \phi_1^{(2)} \cdot \bar{\psi} + (\phi_1^{(3)} + \phi_2^{(3)}) \cdot 0 + \phi_2^{(4)} \cdot \left(-\frac{2}{3} \bar{\psi}\right) + \bar{L}_{\text{obc}} = 0$$

WZORY TRANSFORMACYJNE:

$$\phi_1^{(1)} = \frac{3EJ}{7a} [\varphi_1 - \psi^{(1)}] \quad \phi_1^{(3)} = \frac{2EJ}{10a} [2\varphi_1 + \varphi_2 - 3\psi^{(3)}]$$

$$\phi_1^{(2)} = \frac{3EJ}{5a} [\varphi_1 - \psi^{(2)}] \quad \phi_2^{(3)} = \frac{2EJ}{10a} [\varphi_1 + 2\varphi_2 - 3\psi^{(3)}]$$

$$\phi_2^{(1)} = \frac{3EJ}{6a} [\varphi_2 - \psi^{(1)}]$$

po podstawieniu wzorów transf. do RRMP i przyjęciu

$\bar{\Psi} = -1$ otrzymamy:

$$\frac{EJ}{a} \begin{bmatrix} 10/7 & 1/5 & -207/245 \\ 1/5 & 9/10 & 1/3 \\ -207/245 & 1/3 & 0,962 \end{bmatrix} \begin{bmatrix} \varphi_1 \\ \varphi_2 \\ \psi \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 4 \end{bmatrix} Pa$$

$$\rightarrow \varphi_1 = 11,627 \frac{Pa^2}{EJ} \quad \varphi_2 = -9,070 \frac{Pa^2}{EJ} \quad \psi = 17,513 \frac{Pa^3}{EJ}$$